# Three-dimensional motion of a vortex filament and its relation to the localized induction hierarchy

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**Abstract.** Three-dimensional motion of a slender vortex tube, embedded in an inviscid incompressible fluid, is investigated under the *localized induction approximation* for the Euler equations. Using the method of matched asymptotic expansions in a small parameter  $\epsilon$ , the ratio of core radius to curvature radius, the velocity of a vortex filament is derived to  $O(\epsilon^3)$ , whereby the influence of elliptical deformation of the core due to the self-induced strain is taken into account. It is found that there is an integrable line in the core whose evolution obeys a summation of the first and third terms of the *localized induction hierarchy*.

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## 1 Introduction

An asymptotic theory that concisely spotlights some qualitative behavior of a curved vortex filament in an inviscid incompressible fluid is the so called '*localized induction approximation (LIA)*' [1]. The filament curve  $\mathbf{X} = \mathbf{X}(s, t)$ , expressed as functions of the arclength s and the time t evolves according to

$$\boldsymbol{X}_{t} = C\kappa \boldsymbol{b}; \qquad C = \frac{\Gamma}{4\pi} \log\left(\frac{L}{\sigma_{0}}\right), \qquad (1)$$

where  $\kappa$  is the curvature, **b** the binormal vector,  $\Gamma$  the circulation, and a subscript denotes a differentiation with respect to the indicated variable. The long and short cutoff lengths L and  $\sigma_0$  for the Biot-Savart law and thus C are assumed to be constant.

A distinguishing feature is that (1) is a completely integrable evolution equation equivalent to a cubic nonlinear Schrödinger equation (*NLS*) for the Hasimoto map:

$$\phi(s,t) = \kappa \,\mathrm{e}^{\mathrm{i}\int^s \tau \,\mathrm{d}s},\tag{2}$$

a combination of curvature  $\kappa$  and torsion  $\tau$  [2]. Magri [3] unveiled the bi-Hamiltonian structure behind the integrability of NLS, and manipulated a recursion operator generating successively an infinite sequence of commuting vector fields. Relying on this, Langer and Perline [4] constructed its counterpart for (1). The resulting sequence of integrable vector fields is called the '*localized induction* hierarchy (LIH)'. The first three of them are

$$\boldsymbol{V}^{(1)} = \kappa \boldsymbol{b} , \quad \boldsymbol{V}^{(2)} = \frac{1}{2} \kappa^2 \boldsymbol{t} + \kappa_s \boldsymbol{n} + \kappa \tau \boldsymbol{b} ,$$
$$\boldsymbol{V}^{(3)} = \kappa^2 \tau \boldsymbol{t} + (2\kappa_s \tau + \kappa \tau_s) \boldsymbol{n} + \left(\kappa \tau^2 - \kappa_{ss} - \frac{1}{2}\kappa^3\right) \boldsymbol{b} ,$$
(3)

where (t, n, b) are the Frenet-Serret vectors. Remarkably, when specialized to a circle with constant curvature  $\kappa \neq 0$ and  $\tau = 0$ , a superposition of  $V^{(1)}$  and  $V^{(3)}$  coincides with the higher-order formula for traveling speed of a thin axisymmetric vortex ring [5,6].

This unexpected coincidence inspires us to pursue the higher-order velocity of a vortex filament. We note in passing that the Moore-Saffman filament equation [7], valid to  $O(\epsilon^2)$ , for a vortex filament with axial velocity in the core is reducible to a summation of  $\mathbf{V}^{(1)}$  and  $\mathbf{V}^{(2)}$  [8].

Here, we rule out axial flow at leading order, but make an attempt at an extension of matched asymptotic expansions to  $O(\epsilon^3)$  under the LIA.

## 2 Setting of problem

In order to look into the flow field near the core, it is expedient to introduce local coordinates  $(\tilde{x}, \tilde{y}, \xi)$ , along with local cylindrical coordinates  $(r, \varphi, \xi)$  such that  $\tilde{x} = r \cos \varphi$  and  $\tilde{y} = r \sin \varphi$ , moving with the filament. Here  $\xi$  is a parameter along the central curve  $\boldsymbol{X}$  of the vortex tube,

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defined so as to satisfy  $\dot{\boldsymbol{X}}(\xi,t) \cdot \boldsymbol{t}(\xi,t) = 0$ . Here a dot stands for a derivative in t with fixing  $\xi$ . Given a point  $\boldsymbol{x}$ sufficiently close to the core, there corresponds uniquely the nearest point  $\boldsymbol{X}(\xi,t)$  on the centerline of filament. Then  $\boldsymbol{x}$  is expressed as

$$\boldsymbol{x} = \boldsymbol{X}(\xi, t) + r \cos \varphi \boldsymbol{n} + r \sin \varphi \boldsymbol{b} \,. \tag{4}$$

The coordinates  $(r, \varphi, \xi)$  are converted into orthogonal ones  $(r, \theta, \xi)$  by adjusting the origin of angle as

$$\theta(\varphi,\xi,t) = \varphi - \int_{s_0}^{s(\xi,t)} \tau(s',t) \,\mathrm{d}s' \,, \tag{5}$$

where  $s = s(\xi, t)$  is the arclength along the centerline [7].

We define the relative velocity  ${\pmb V}=(u,v,w)$  as functions of  $r,\theta,\xi$  and t by

$$\boldsymbol{v} = \boldsymbol{X}(\boldsymbol{\xi}, t) + u\boldsymbol{e}_r + v\boldsymbol{e}_\theta + w\boldsymbol{t}, \qquad (6)$$

where  $e_r$  and  $e_{\theta}$  are the unit vectors in the radial and azimuthal directions respectively. The vorticity  $\boldsymbol{\omega} = \nabla \times \boldsymbol{v}$ is calculated through

$$\boldsymbol{\omega} = \omega_r \boldsymbol{e}_r + \omega_\theta \boldsymbol{e}_\theta + \zeta \boldsymbol{t} \tag{7}$$

$$= \left\{ \frac{1}{r} \frac{\partial w}{\partial \theta} - \frac{1}{h_3} \frac{\partial v}{\partial \xi} + \frac{\eta}{h_3} \kappa w \sin \varphi - \frac{1}{h_3} \frac{\partial \dot{\mathbf{X}}}{\partial \xi} \cdot \mathbf{e}_\theta \right\} \mathbf{e}_r$$
$$+ \left\{ -\frac{\partial w}{\partial r} + \frac{1}{h_3} \frac{\partial u}{\partial \xi} + \frac{\eta}{h_3} \kappa w \cos \varphi + \frac{1}{h_3} \frac{\partial \dot{\mathbf{X}}}{\partial \xi} \cdot \mathbf{e}_r \right\} \mathbf{e}_\theta$$
$$+ \left\{ \frac{1}{r} \frac{\partial}{\partial r} (rv) - \frac{1}{r} \frac{\partial u}{\partial \theta} \right\} \mathbf{t},$$
(8)

where

$$\eta = |\partial \boldsymbol{X} / \partial \xi|, \quad h_3 = \eta (1 - \kappa r \cos \varphi).$$
 (9)

We are concerned with a *quasi-steady* motion of a vortex filament. Suppose that the leading-order flow is circulatory motion with prescribed velocity field  $v^{(0)}(r)$  as a function only of r. Consistently with the LIA, we may pose the following form for the perturbation solution in a power series in  $\epsilon = \sigma_0/R_0$ , the ratio of a typical core radius  $\sigma_0$  to a typical curvature radius  $R_0$ :

$$u = \epsilon u^{(1)} + \epsilon^2 u^{(2)} + \epsilon^3 u^{(3)} + \cdots,$$
  

$$v = v^{(0)}(r) + \epsilon v^{(1)} + \epsilon^2 v^{(2)} + \epsilon^3 v^{(3)} + \cdots,$$
  

$$w = \epsilon^2 w^{(2)} + \cdots, \quad \dot{\mathbf{X}} = \dot{\mathbf{X}}^{(0)} + \epsilon^2 \dot{\mathbf{X}}^{(2)} + \cdots.$$
(10)

Inspection from (8) and (10) tells us that

$$\omega_r = \epsilon^2 \omega_r^{(2)} + \cdots, \quad \omega_\theta = \epsilon^2 \omega_\theta^{(2)} + \cdots,$$
  
$$\zeta = \zeta^{(0)}(r) + \epsilon \zeta^{(1)} + \epsilon^2 \zeta^{(2)} + \epsilon^3 \zeta^{(3)} + \cdots. \quad (11)$$

To integrate the Euler equations, it is advantageous to eliminate the pressure at the outset and to deal exclusively with vorticity and vector potential  $\boldsymbol{A}$  for the velocity:  $\boldsymbol{v} = \nabla \times \boldsymbol{A}$ . Introduce a Stokes streamfunction

$$\psi(\boldsymbol{x}) = (1 - \kappa r \cos \varphi) \boldsymbol{A}(\boldsymbol{x}) \cdot \boldsymbol{t}(\xi)$$
(12)

$$=\psi^{(0)}(r) + \epsilon\psi^{(1)} + \epsilon^2\psi^{(2)} + \epsilon^3\psi^{(3)} + \cdots,$$
(13)

for the flow in the plane transversal to t.

### 3 Asymptotic development of Biot-Savart law

This section presents only a brief sketch of how to perform an asymptotic development, valid near the core, of the Biot-Savart law for A(x).

The vorticity is dominated by the tangential contribution  $\zeta$ . We stipulate that  $|\zeta|$  decays sufficiently rapidly to zero with distance r from the vortex centerline. The contribution  $A_{\parallel}$  from  $\zeta$  is

$$\boldsymbol{A}_{\parallel}(\boldsymbol{x}) = \frac{1}{4\pi} \iiint \frac{\zeta(\tilde{x}, \tilde{y})\boldsymbol{t}(s)(1-\kappa\tilde{x})}{|\boldsymbol{x}-\boldsymbol{X}-\tilde{x}\boldsymbol{n}-\tilde{y}\boldsymbol{b}|} \,\mathrm{d}\tilde{x}\mathrm{d}\tilde{y}\mathrm{d}s \,. \tag{14}$$

Use of a shift-operator, being adapted from Dyson's technique [5], facilitates to rewrite (14) in a form amenable to a multi-pole expansion as

$$\mathbf{A}_{\parallel}(\boldsymbol{x}) = \frac{1}{4\pi} \int \mathrm{d}s \left\{ \iint \mathrm{d}\tilde{x} \mathrm{d}\tilde{y}\zeta(\tilde{x},\tilde{y})(1-\kappa\tilde{x}) \right. \\ \left. \times \exp\left[-\tilde{x}(\boldsymbol{n}\cdot\nabla) - \tilde{y}(\boldsymbol{b}\cdot\nabla)\right] \right\} \frac{\boldsymbol{t}(s)}{|\boldsymbol{x} - \boldsymbol{X}(s)|}$$
(15)

$$= \frac{1}{4\pi} \int ds \left\{ \iint d\tilde{x} d\tilde{y} \zeta \left( 1 - \kappa \tilde{x} - \tilde{x} (\boldsymbol{n} \cdot \nabla) - \tilde{y} (\boldsymbol{b} \cdot \nabla) \right. \\ \left. + \frac{1}{2} \left[ \tilde{x}^2 (\boldsymbol{n} \cdot \nabla)^2 + 2 \tilde{x} \tilde{y} (\boldsymbol{n} \cdot \nabla) (\boldsymbol{b} \cdot \nabla) + \tilde{y}^2 (\boldsymbol{b} \cdot \nabla)^2 \right] \right. \\ \left. + \kappa \tilde{x}^2 (\boldsymbol{n} \cdot \nabla) + \kappa \tilde{x} \tilde{y} (\boldsymbol{b} \cdot \nabla) + \cdots \right) \right\} \frac{\boldsymbol{t}(s)}{|\boldsymbol{x} - \boldsymbol{X}(s)|} \cdot$$
(16)

We shall know from the inner expansion in Section 4 the following dependence of  $\zeta$  on  $\varphi$ :

$$\zeta(\tilde{x}, \tilde{y}) = \zeta_0 + \zeta_{11} \cos \varphi + \zeta_{12} \sin \varphi + \zeta_{21} \cos 2\varphi + \cdots,$$
(17)

where

$$\zeta_0 \approx \zeta^{(0)}(r) + \kappa^2 \hat{\zeta}_0^{(2)}(r) , \quad \zeta_{11} \approx \kappa \hat{\zeta}_{11}^{(1)}(r) + \kappa^3 \hat{\zeta}_{11}^{(3)}(r) ,$$
  

$$\zeta_{12} \approx \kappa \hat{\zeta}_{12}^{(1)}(r) , \quad \zeta_{21} \approx \kappa^2 \hat{\zeta}_{21}^{(2)}(r) .$$
(18)

In  $\hat{\zeta}_{ij}^{(k)}$ , the superscript k stands for order of perturbation, and i labels the Fourier mode with j = 1 and 2 being corresponding to  $\cos i\theta$  and  $\sin i\theta$  respectively.

Substituting (17) and (18) into (16), we get the first two terms  $A_m$  and  $A_{\parallel d}$  as

$$\boldsymbol{A}_{\parallel}(\boldsymbol{x}) = \boldsymbol{A}_{m}(\boldsymbol{x}) + \boldsymbol{A}_{\parallel d}(\boldsymbol{x}) + \cdots, \qquad (19)$$

 $\psi$ 

where

$$\boldsymbol{A}_{m}(\boldsymbol{x}) = \frac{\Gamma}{4\pi} \int \frac{\boldsymbol{t}(s)}{|\boldsymbol{x} - \boldsymbol{X}(s)|} \mathrm{d}s ,$$
  
$$\boldsymbol{A}_{\parallel d}(\boldsymbol{x}) = -\frac{1}{16\pi} \left[ 2\pi \int_{0}^{\infty} r^{3} \zeta^{(0)} \mathrm{d}r \right] \int \frac{\kappa_{s} \boldsymbol{n} + \kappa \tau \boldsymbol{b}}{|\boldsymbol{x} - \boldsymbol{X}(s)|} \mathrm{d}s$$
  
$$-\frac{d^{(1)}}{2} \int \mathrm{d}s \left[ \kappa (\boldsymbol{n} \cdot \nabla) + \kappa^{2} \right] \frac{\boldsymbol{t}}{|\boldsymbol{x} - \boldsymbol{X}(s)|} , (20)$$

with

ω

$$d^{(1)} = \frac{1}{4\pi} \left\{ \left[ 2\pi \int_0^\infty r^2 \hat{\zeta}_{11}^{(1)} \mathrm{d}r \right] - \frac{1}{2} \left[ 2\pi \int_0^\infty r^3 \zeta^{(0)} \mathrm{d}r \right] \right\},$$
(21)

being the strength of dipole.

The first term  $A_m$  in (19) pertains to a flow field induced by a curved vortex line of infinitesimal thickness, and is called the 'monopole field'. The correction term  $A_{\parallel d}$ corresponds to a part of the flow field induced by a line of dipoles, based at the vortex centerline, with their axes oriented in the binormal direction. The origin of dipole field is attributable to the curvature effect; by bending a vortex tube, the vortex lines on the convex side are stretched, while those on the concave side are contracted, producing effectively a vortex pair [6].

The components of vorticity perpendicular to t make its appearance at  $O(\epsilon^2)$ . In view of (8), the second-order terms  $\omega_r^{(2)}$  and  $\omega_{\theta}^{(2)}$  are expressible as

$$\omega_r^{(2)} = \frac{\zeta^{(0)}}{v^{(0)}} \hat{\psi}_{11}^{(1)} (\kappa_s \cos \varphi + \kappa \tau \sin \varphi) \,, \tag{22}$$

$$\psi_{\theta}^{(2)} = \frac{r\zeta^{(0)}}{v^{(0)}} \left[ \left( \frac{2}{r} - \frac{\zeta^{(0)}}{v^{(0)}} \right) \hat{\psi}_{11}^{(1)} + \frac{\partial \hat{\psi}_{11}^{(1)}}{\partial r} - rv^{(0)} \right] \\
\times (\kappa\tau \cos\varphi - \kappa_* \sin\varphi),$$
(23)

where  $\hat{\psi}_{11}^{(1)}$  will be determined as (29) in Section 4. The vector potential  $\mathbf{A}_{\perp}$  associated with the transversal vorticity is, to  $O(\epsilon^2)$ ,

$$\boldsymbol{A}_{\perp}(\boldsymbol{x}) \approx \frac{1}{4\pi} \int \frac{\mathrm{d}s}{|\boldsymbol{x} - \boldsymbol{X}(s)|} \left[ \iint (\omega_r \boldsymbol{e}_r + \omega_\theta \boldsymbol{e}_\theta) \mathrm{d}\tilde{x} \mathrm{d}\tilde{y} \right].$$
(24)

Substitution from (22) and (23) yields

$$\boldsymbol{A}_{\perp} \approx \frac{1}{4} \left[ \int_0^\infty r^2 \hat{\zeta}_{11}^{(1)} \mathrm{d}r \right] \int \frac{\kappa_s(s) \boldsymbol{n}(s) + \kappa(s) \tau(s) \boldsymbol{b}(s)}{|\boldsymbol{x} - \boldsymbol{X}(s)|} \mathrm{d}s \,,$$
(25)

the *dipole field* originating from the transversal vorticity. Collecting (20) and (25), we have

$$\boldsymbol{A} \approx \frac{\Gamma}{4\pi} \int \frac{\boldsymbol{t}}{|\boldsymbol{x} - \boldsymbol{X}|} \mathrm{d}\boldsymbol{s} - \frac{d^{(1)}}{2} \int \frac{\kappa \boldsymbol{b} \times (\boldsymbol{x} - \boldsymbol{X})}{|\boldsymbol{x} - \boldsymbol{X}|^3} \mathrm{d}\boldsymbol{s} \,. \, (26)$$

The tangential component  $\psi$  defined by (12) is evaluated near the core ( $\sigma_0 \ll r \ll R_0$ ), which in turn supplies the matching condition on the inner solution. Retaining only the terms with  $\log(L/r)$ , in the spirit of LIA, and the dipole term, for clarity, we have

$$(\boldsymbol{x}) = d^{(1)} \kappa \frac{\cos \varphi}{r} + \log \left(\frac{L}{r}\right) \left\{ \frac{\Gamma}{2\pi} \left(1 - \frac{\kappa}{2} r \cos \varphi\right) + \frac{1}{16\pi} \kappa^2 \left[ \Gamma \left(1 - \frac{1}{2} \cos 2\varphi\right) r^2 - 2d^{(1)} \right] + \frac{\Gamma}{32\pi} \left[ \left(\frac{3\kappa^3}{4} - \kappa_{ss} + \kappa\tau^2\right) \cos \varphi - \frac{\kappa^3}{4} \cos 3\varphi - (2\kappa_s\tau + \kappa\tau) \sin \varphi \right] r^3 + \frac{d^{(1)}}{2} \left[ \left(-\frac{\kappa^3}{4} + \kappa_{ss} - \kappa\tau^2\right) \cos \varphi + (2\kappa_s\tau + \kappa\tau_s) \sin \varphi \right] r \right\} + \cdots .$$

$$(27)$$

## 4 Inner solution and filament equation

The inner solution is addressed by solving the Euler equations in the moving coordinates. We introduce the dimensionless variables; the radial distance r is normalized by  $\sigma_0$ , the core radius, time by  $R_0^2/\Gamma$ , the relative velocity by  $\Gamma/\sigma_0$  and the centerline velocity by  $\Gamma/R_0$ . With this, we write down dimensionless form of the Euler equations and their curl, viewed from the moving coordinates  $(r, \theta, \xi)$ , along with the subsidiary relation that links  $\psi$ to  $\zeta$ .

The solution at  $O(\epsilon)$  is well-known [9–11]:

$$\psi^{(1)} = \left[\kappa \hat{\psi}_{11}^{(1)} - \left(\dot{\boldsymbol{X}}^{(0)} \cdot \boldsymbol{b}\right) r\right] \cos\varphi, \qquad (28)$$

where

$$\hat{\psi}_{11}^{(1)} = v^{(0)} \left\{ \frac{r^2}{2} + \int_0^r \frac{\mathrm{d}r'}{r'[v^{(0)}(r')]^2} \int_0^{r'} r'' \left[ v^{(0)}(r'') \right]^2 \mathrm{d}r'' \right\} + c_{11}^{(1)} v^{(0)}, \tag{29}$$

and  $c_{11}^{(1)}$  is a constant bearing with the freedom of shift-ing the local origin r = 0 of the moving frame, in the *n*-direction, within an accuracy of  $O(\epsilon)$  [6]. The matching condition (27) at  $O(\epsilon)$  then demands the LIA (1) for  $\dot{\boldsymbol{X}}^{(0)}$ . The vorticity at  $O(\epsilon)$  is calculable through

$$\zeta^{(1)} = -\kappa \left( a \hat{\psi}_{11}^{(1)} + r \zeta^{(0)} \right) \cos \varphi \,. \tag{30}$$

Fortunately an explicit form of  $p^{(1)}$  is available by integrating the transversal components of the Euler equations:

$$p^{(1)} = \kappa \left[ v^{(0)} \frac{\partial \hat{\psi}_{11}^{(1)}}{\partial r} - \zeta^{(0)} \hat{\psi}_{11}^{(1)} - r(v^{(0)})^2 \right] \cos \varphi \,. \tag{31}$$

The gradient of  $p^{(1)}$ , in turn, drives axial flow at  $O(\epsilon^2)$ . Discarding the irrelevant terms from the *t*-component of the Euler equations, we obtain

$$-v^{(0)}(\boldsymbol{e}_{\theta}\cdot\dot{\boldsymbol{t}}^{(0)}) + \frac{v^{(0)}}{r}\frac{\partial w^{(2)}}{\partial \theta} = -\frac{1}{\eta}\frac{\partial p^{(1)}}{\partial \xi} \cdot \qquad (32)$$

A derivative in t of (1) gives

$$\boldsymbol{e}_{\theta} \cdot \dot{\boldsymbol{t}}^{(0)} = C(\kappa_s \cos \varphi + \kappa \tau \sin \varphi),$$
 (33)

and (32) admits a compact form of the solution:

$$w^{(2)} = \left\{ -C\kappa + \frac{\partial \hat{\psi}_{11}^{(1)}}{\partial r} - \frac{\zeta^{(0)}}{v^{(0)}} \hat{\psi}_{11}^{(1)} - rv^{(0)} \right\} r$$
$$\times (\kappa\tau \cos\varphi - \kappa_s \sin\varphi) \,. \tag{34}$$

We observe from (34) that torsion and arcwise variation of curvature are vital for the presence of pressure gradient and thus of axial velocity at  $O(\epsilon^2)$ . The streamfunction  $\psi^{(2)}$  at  $O(\epsilon^2)$  for flow in the transversal plane is built in parallel with the case of a circular vortex ring [6].

We are now prepared to make headway to third order. The terms proportional to  $\kappa^3$  in  $\dot{\boldsymbol{X}}^{(2)}$  are in complete agreement with those for a circular vortex ring [6]. Hence it suffices to concentrate our attention on the terms tied with torsion and non-constancy of curvature. Retaining only the terms associated with these three-dimensional effects in the vorticity equation at  $O(\epsilon^3)$ , we are left with

$$\dot{\zeta}^{(1)} - \left(\dot{\boldsymbol{e}}_{r}^{(0)} \cdot \boldsymbol{e}_{\theta}\right) \frac{\partial \zeta^{(1)}}{\partial \theta} + \frac{v^{(0)}}{r} \frac{\partial \zeta^{(3)}}{\partial \theta} + u^{(3)} \frac{\partial \zeta^{(0)}}{\partial r} + \dots = \frac{\zeta^{(0)}}{\eta} \frac{\partial w^{(2)}}{\partial \xi} + \left(\zeta^{(1)} + \kappa r \cos \varphi \zeta^{(0)}\right) \frac{\boldsymbol{t}}{\eta} \cdot \frac{\partial \dot{\boldsymbol{X}}^{(0)}}{\partial \xi} + \dots, \quad (35)$$

the last two terms of which vanish because of (1). The third-order velocity  $\dot{\mathbf{X}}^{(2)}$  under question is included in  $\zeta^{(3)}$  and  $u^{(3)}$ . Relevant to the traveling speed is the terms proportional to  $\cos \varphi$  and  $\sin \varphi$ , the dipole components.

The first term  $\dot{\zeta}^{(1)}$  is obtained from (30) as

$$\dot{\zeta}^{(1)} = -\left(a\hat{\psi}_{11}^{(1)} + r\zeta^{(0)}\right)\left(\dot{\kappa}^{(0)}\cos\varphi + \kappa\dot{T}^{(0)}\sin\varphi\right)\,,\tag{36}$$

where

$$T(\xi, t) = \int_0^{s(\xi, t)} \tau(s', t) \,\mathrm{d}s' \,, \tag{37}$$

and  $\dot{\kappa}^{(0)}$  and  $\dot{T}^{(0)}$  are substituted from the intrinsic form of (1) [1]. Likewise we have

$$\dot{\boldsymbol{e}}_{r}^{(0)} \cdot \boldsymbol{e}_{\theta} = C\left(\frac{\kappa_{ss}}{\kappa} - \tau^{2}\right) - \dot{T}^{(0)}.$$
(38)

With these, (35) is integrated for  $\zeta^{(3)}$  and is coupled to  $\zeta - \psi$  relation at  $O(\epsilon^3)$ . Imposition of the matching condition (27) eventually gives rise to the third-order correction  $\dot{\boldsymbol{X}}^{(2)}$ . Combining with (1), we arrive at a higher-order extension expressed, in dimensional variables, as

$$\boldsymbol{X}_{t} = C \left\{ \kappa \boldsymbol{b} + c_{1} \kappa^{3} \boldsymbol{b} + c_{2} \left[ (2\kappa_{s} \tau + \kappa \tau_{s}) \boldsymbol{n} + (\kappa \tau^{2} - \kappa_{ss}) \boldsymbol{b} + \kappa^{2} \tau \boldsymbol{t} \right] \right\},$$
(39)

where

i

$$c_1 = \frac{2\pi d^{(1)}}{\Gamma}, \quad c_2 = \frac{\pi}{\Gamma} \int_0^\infty \zeta^{(0)} r^3 \mathrm{d}r.$$
 (40)

The Hasimoto map (2) transforms (39) into

$$\begin{aligned} \ddot{\phi}_{t} + C\left(\phi_{ss} + \frac{1}{2}|\phi|^{2}\phi\right) + A(t)\phi - Cc_{2}\left\{\phi_{ssss}\right. \\ &+ \frac{3}{2}\left(|\phi|^{2}\phi_{ss} + \phi_{s}^{2}\bar{\phi}\right) + \left(\frac{3}{8}|\phi|^{4} + \frac{1}{2}\frac{\partial^{2}}{\partial s^{2}}|\phi|^{2}\right)\phi\right\} \\ &+ C\left(c_{1} + \frac{c_{2}}{2}\right)\left\{\frac{\partial^{2}}{\partial s^{2}}(|\phi|^{2}\phi) + \frac{3}{4}|\phi|^{4}\phi\right\} = 0, \quad (41)\end{aligned}$$

where A(t) is an arbitrary function of t. Interestingly equivalent equations have been realized in the context of biquadratic Heisenberg spin chain [12]. The simple form (40) of  $c_1$  is derived by reducing further the formula for a vortex ring [6]. Its derivation will be reported elsewhere.

We see that the third-order correction terms closely resemble  $V^{(3)}$ . The special case of  $c_1 = -c_2/2$  attains integrability. Remember that the dipole strength  $d^{(1)}$  and therefore  $c_1$  are sensitive to location of the origin r = 0 of the moving coordinates [6]; by a displacement of origin in the **n**-direction by  $\epsilon x_0$ , measured in the inner length-scale,

$$d^{(1)} \to d^{(1)} - x_0/2\pi, \quad c_1 \to c_1 - x_0.$$
 (42)

It is confirmed that  $c_1$  is adjustable so as to be coincident with  $V^{(3)}$ , and that the local origin for this case is indeed contained inside the core. We conclude that there is an *integrable line* that obeys a summation of the first and the third terms of the LIH.

This fact is illustrated with a specific vorticity distribution at  $O(\epsilon^0)$  of constant vorticity in the circular core, that is, the *Rankine vortex*. The azimuthal velocity at  $O(\epsilon^0)$  takes, in dimensionless variables,

$$v^{(0)} = \frac{r}{2\pi}$$
 for  $r \le 1$ ;  $v^{(0)} = \frac{1}{2\pi r}$  for  $r > 1$ . (43)

Choosing  $c_{11}^{(1)} = -5/8$  amounts to placing the local origin r = 0 at the center of core circle, and, from (21),  $d^{(1)} = -3/16\pi$ . In this case  $x_0 = 0$ . For a general value of  $x_0$ , the third-order terms of (39) become

$$\frac{C}{4} \left\{ (2\kappa_s \tau + \kappa \tau_s) \boldsymbol{n} + \left[ \kappa \tau^2 - \kappa_{ss} - \left(\frac{3}{2} + 4x_0\right) \kappa^3 \right] \boldsymbol{b} + \kappa^2 \tau \boldsymbol{t} \right\}.$$
(44)

Recall that the choice of  $x_0 = -5/8$  corresponds to placing the origin r = 0 at the stagnation point relative to the moving frame. Choice of  $x_0 = -1/4$ , a value between  $x_0 = -5/8$  and 0, renders (39) and (41) completely integrable.

We have extended the matched asymptotic expansions, to third order, for the motion of a vortex filament. This amounts to taking account of finite thickness of the core. The preservation of integrability to third order is indicative of structural stability of the Hasimoto soliton.

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